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ANGLASSIE

Major Caliber HC Projectiles

PART A

SYNOPSIS

- 1. This test was conducted to determine the fragmentation characteristics of 12" Mk 17 and 14" Mk 19 HC projectiles, Explosive "D" loaded.
- 2. a. The 12" HC projectile when compared to the 14" HC projectile produced about 35% more fragments weighing 2-1/2 to 640 grams and considerably less fragments weighing over 640 grams in polar angle zone 60° 120°. About 85% of the projectile fragment weight of either projectile was expelled in zone 60° 120°.
- b. The 12" and 14" projectiles produced average median beam spray fragment velocities of 2140 ft/sec and 2210 ft/sec respectively.



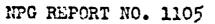


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PART B

INTRODUCTION

AUTHORITY: 1.

This test was authorized by reference (a) and conducted under Task Assignment NPG-36-Re3d-418-1 which was renewed by Task Assignment NPG-Re3d-418-1-53, reference (b).

REFERENCES:

- BUORD Conf 1tr \$78-1(117) Re3d ANB:bc of 14 June 1949
- BUORD 1tr NP9 Re3d-ANB: bc of 29 July 1952 NPG Conf TelCon to BUORD 578-1(66-1) TZ:VW:ldd of 21 June 1950
- BUORD Conf 1tr 578-1(117) Re3d-AHM: bc Ser 46693 of d. 24 October 1952
- NPG Report No. 129 of 19 October 1948

3. BACKGROUND:

a. Reference (a) requested that fragmentation tests of 12", 14", and 16" HC projectiles be conducted over the water pit with the projectiles in horizontal, base down and nose down positions. The tests requiring base down and nose down positions of the 14" and 16" projectiles were cancelled by reference (c) and the horizontal position test of the 16" projectile was cancelled by reference (d). This action was taken because of fragment hazard to nearby Naval Proving Ground installations and the possibility of damage to privately owned property.

b- Base fragment velocities of projectiles, 3" through 16", are being determined and will be the subject of a separate report.

4. OBJECT OF TEST:

This test was conducted to determine the fragmentation characteristics of 12" Mk 17 and 14" Mk 19 HC projectiles, Explosive "D" loaded.



5. PERIOD OF TEST:

a. Dates Project Letters	14 June 1949 21 June 1950 24 October 1952
b. Date Necessary Material Received	15 June 1949
c. Date Commenced Test	28 October 1949
d. Test Firing Completed (12" and 14")	14 June 1950
e. 16" Firing Cancelled	24 October 1952

PART C

DETAILS OF TEST

6. Description of Item under test:

a. 12" HC projectiles, Mk 17 Mod 2, Lot 4, Explosive "D" loaded and assembled with Mk 55 ADF and Mk 29 PDF, both modified for static detonation.

b. 14" HC projectile, Nk 19 Mod 4, Lot 13, Explosive "D" loaded and assembled with Nk 55 ADF and Mk 29 PDF, both modified for static detonation.

c. The projectile and explosive weights are as follows:

Rd.	troi.	Firing Position	Empty and fuzed wt. (1bs)	Exp. "D" wt. (1bs)	Total wt. (1bs)	Frag. No.
1	12"	Horizontal	856.8	79.4	936.2	1421
2	11	11	855.8	11	935.2	1422
. 3	11	11	855.8 854.8	**	934.2	1423
3	H į	Base Down	854.8	11	934.2	1425
5	11	Nose Down	856.8	11	936.2	1429
1	14"	Horizontal	1170.0	104.2	1274.2	1450
2	***	. 11	1164.2	11	1268.4	1460
3	11	1f	1168.1	41	1272.3	1479

7. DESCRIPTION OF TEST EQUIPMENT:

- a. Water Pit: A 15' square opening at ground level leading into a 20' square by 10' deep chamber filled with water. Projectiles are suspended directly above the opening by the use of a horizontal beam, such that (1) if the projectile is in a horizontal position, 1/6 of the fragments in the zone 60° -120° are trapped in the water pit, (2) if the projectile is suspended in a nose down position, all of the fragments in the zone 0° -30° are trapped in the water pit, and (3) if the projectile is suspended in a base down position, all of the fragments in the zone 150° 180° are trapped in the water pit. All zones are polar angle zones measured from the nose, 0°.
- b. 20' high vertical steel panels 80' from the projectile in zone 91° 104° were utilized for fragment velocity determinations along with a 35mm Fastax Camera. A photograph of the water pit set up is shown in Figure 1.

8. RESULTS AND DISCUSSION:

a. Mass distribution for zone 60° - 120°: The recovered fragments are shown in Figures 2 to 9, inclusive, and the detailed mass distribution data are listed in Tables I and II. The summarized data are as follows:

Fragment	1/	6 of Total No. Fragment	s in Zone 60° - 120°.
wt. group (grams)	Rd. 1	12" HC Rd. 2 & Rd. 3 average	Rds. 1. 2. & 3 avorage
2-1/2 - 10 10 - 40 40 - 160 160 - 640 640 +	567 437 316 72 1	184 148 150 87	99 118 112 82 35

Round No. 1 of the 12" HC projectile had a much finer fragment mass distribution than Rounds Nos. 2 and 3 and was not used in averaging the data. Metallurgical examination of the fragments of these projectiles (Appendix (D)) indicated that the only difference in properties was the distinctly greater brittleness of Round No. 1, as evidenced by the Charpy tost. It is well known that a more brittle case material tends to give a finer fragmentation; for example, cast iron. Reference (e) indicated that the increased brittleness of a 5" projectile body caused by a decrease in its temperature was

reflected in a finer fragmentation. The anomalous results observed for Round No. 1 are therefore attributed to its brittleness. The 12" HC projectile (excluding Round No. 1) produced approximately 35% more fragments weighing 2-1/2 to 640 grams than the 14" HC projectile in polar angle zone 60° - 120°. About 85% of the projectile fragment weight of either projectile was expelled in zone 60° - 120°.

b. Mass distribution for zones 0° - 30° and 150° - 180°: The 0° - 30° fragments represent 1-1/2% and the 150° - 180° fragments represent 6-1/2% of the projectile fragment weight. The summarized data are as follows:

Fragmont Weight Group		Fragments HC
(grams)	0° - 30°	150° - 180°
2-1/2 - 10	8	200
10 - 40	8	96
40 - 160	5	36
160 - 640	9	41
640 +	1	5

c. Fragment velocity: The detailed beam spray, 91° - 104°, fragment velocity data listed in Tables III and IV are summarized as follows:

	Median Fragment	Volocity (ft/soc)
Rd. No.	Is" HC	14" HC
ı	2110	
2	2130	2230
3	2170	2290
Avorage	2140	2210

The above velocities are a mean measured over the first 80 feet of travel.

PART D

CONCLUSIONS

- 9. a. The 12" HC projectile when compared to the 14" HC projectile produced about 35% more fragments weighing 2-1/2 to 640 grams and considerably less fragments weighing over 640 grams in polar angle zone 60° 120°. About 85% of the projectile fragment weight of either projectile was expelled in zone 60° 120°.
- b. The 12" and 14" projectiles produced average median beam spray fragment velocities of 2140 ft/sec and 2210 ft/sec respectively.

The tests upon which this report is based were conducted by: V. WILSON, Lieutenant, USN, Fragmentation Firing Officer Fragmentation Division

Terminal Ballistics Department

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E. A. RUCKNER

Captain, USN

Ordnance Officer

By direction

U. S. NAVAL PROVING GROUND DAHLGREN, VIRGINIA

Twenty-first Partial Report

cn

Fragmentation Characteristics

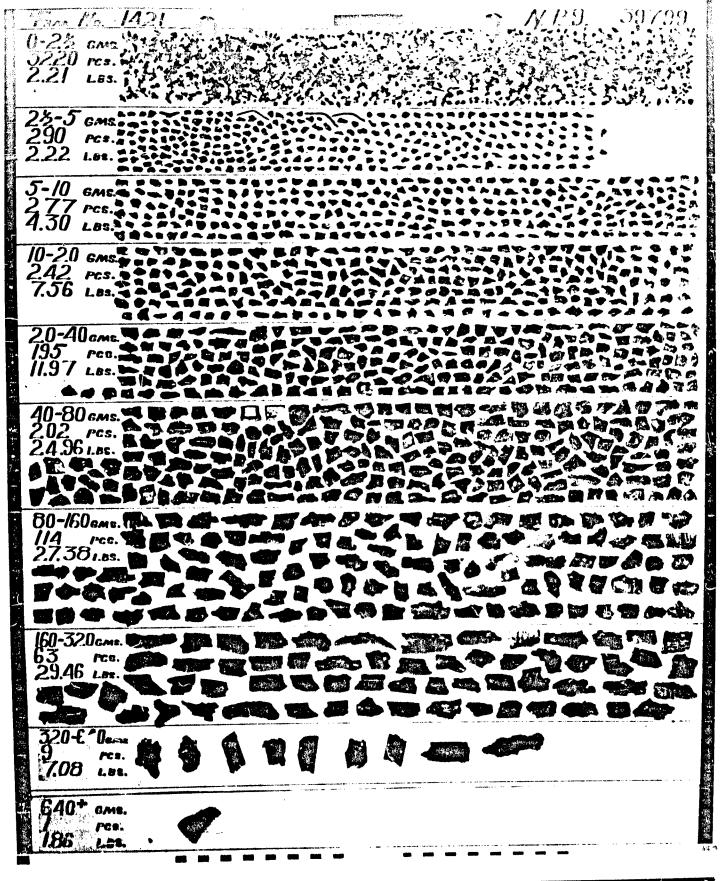
Final Report

on

Major Celiber HC Projectiles

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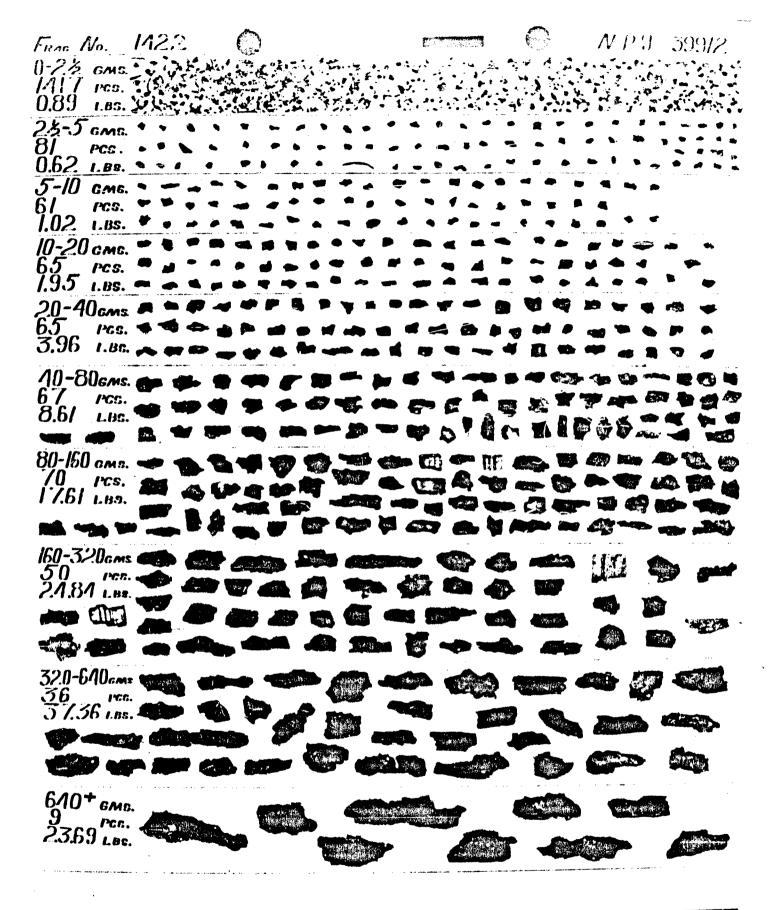
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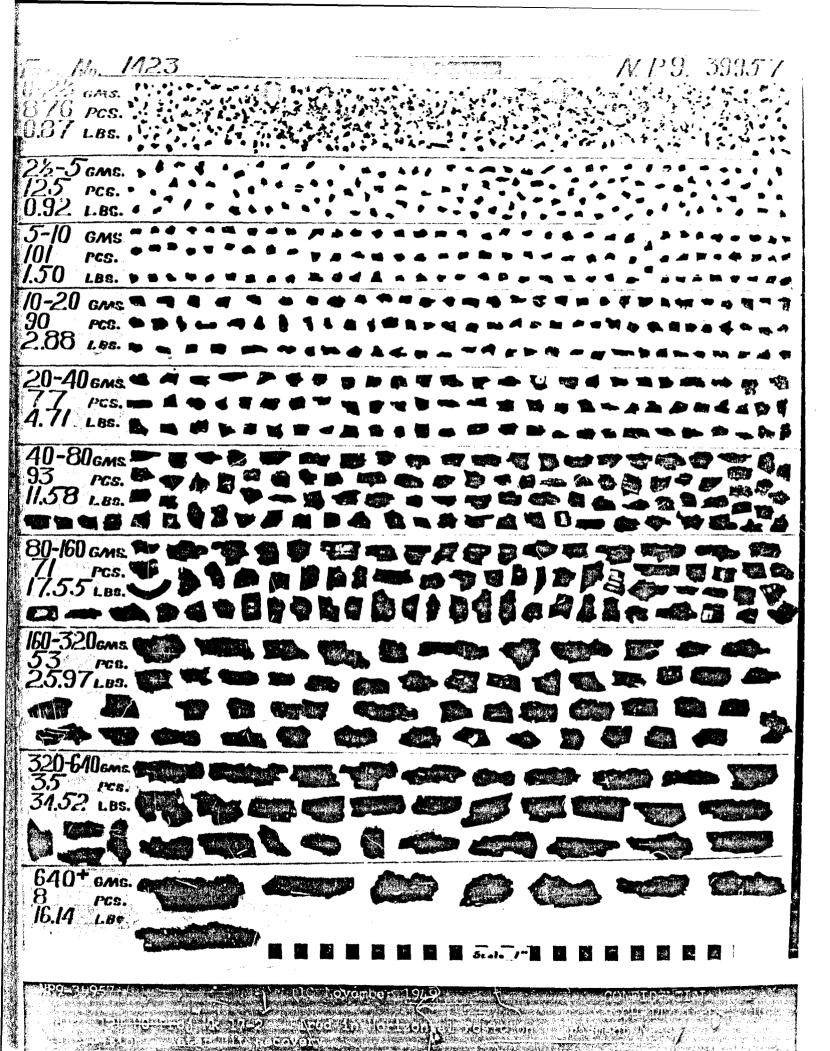
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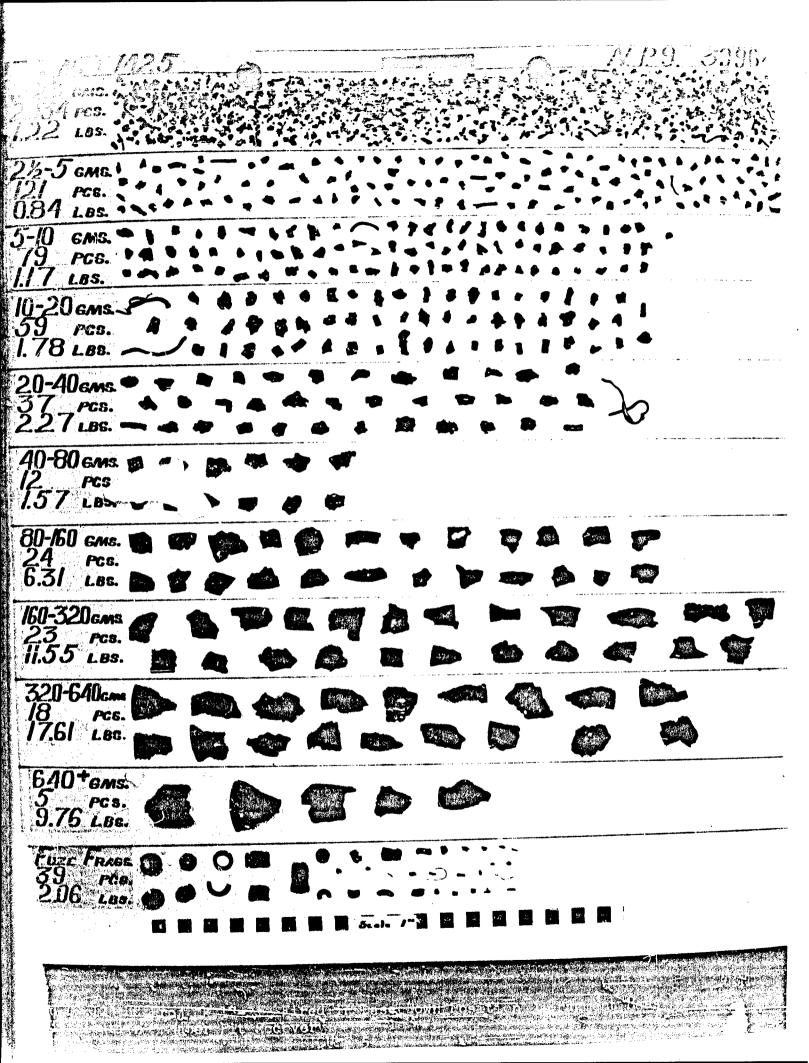
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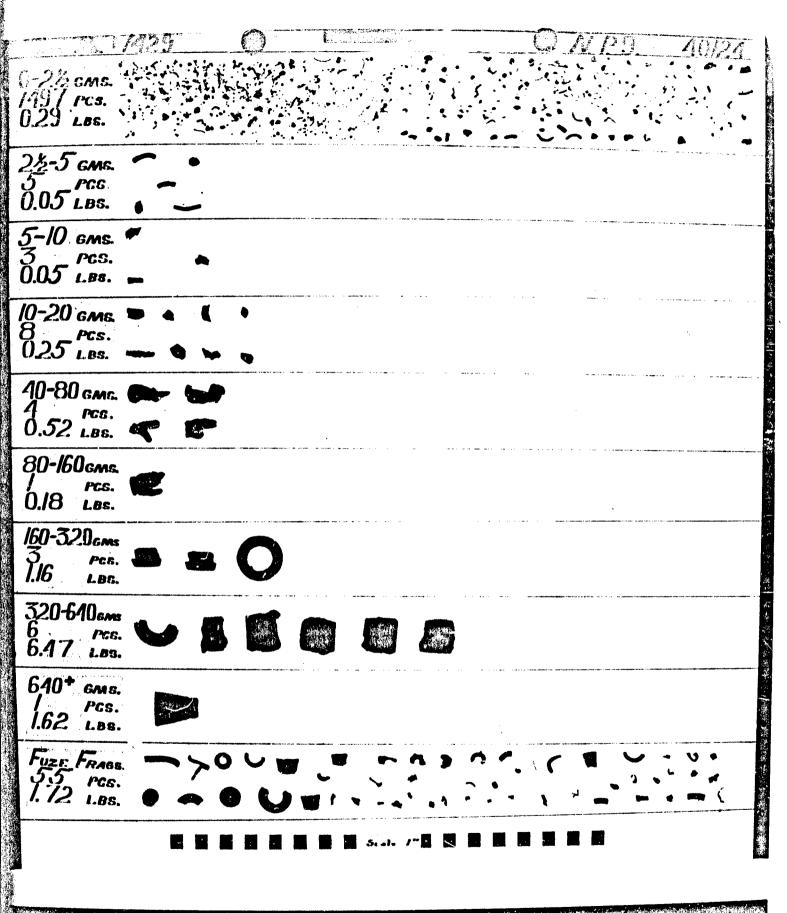
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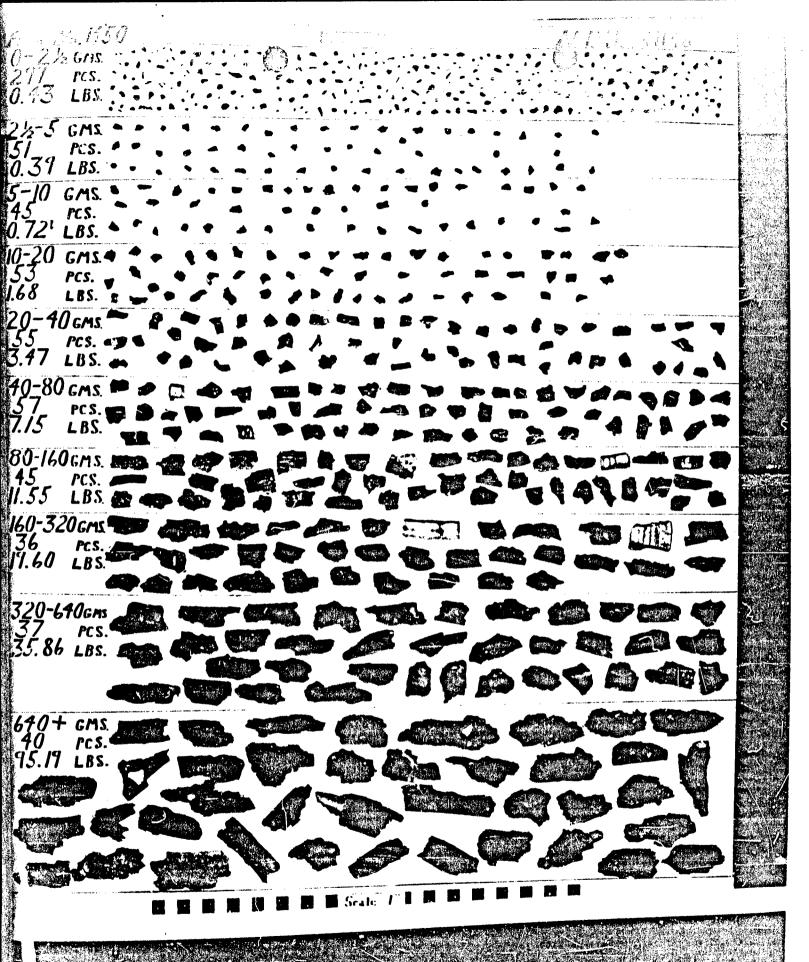
FIGURES



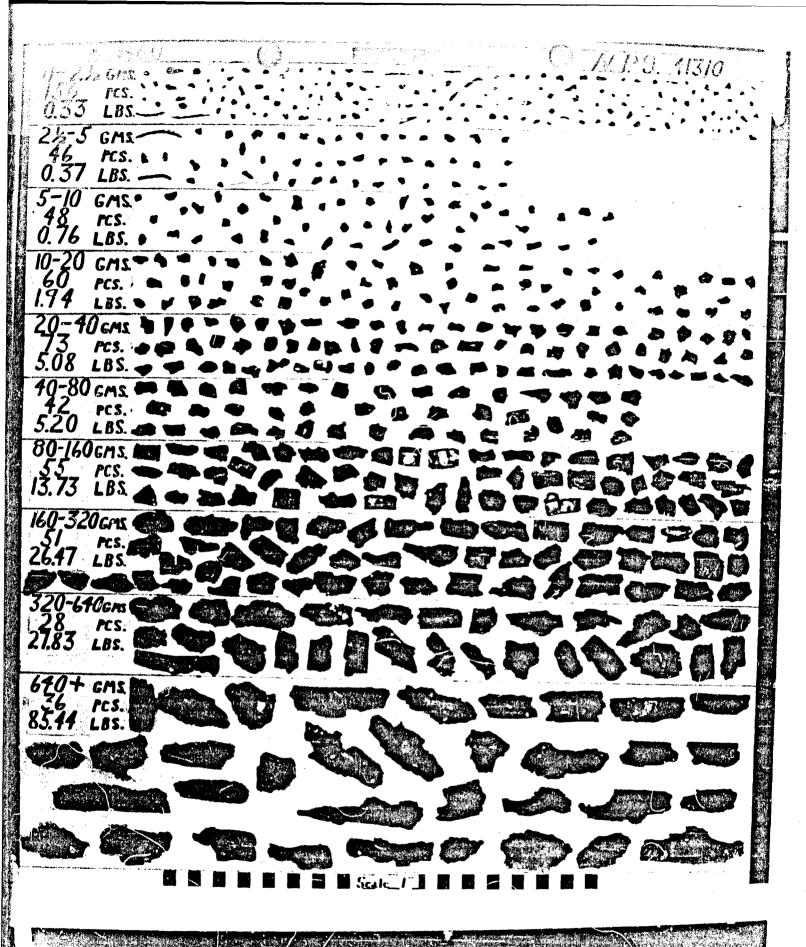




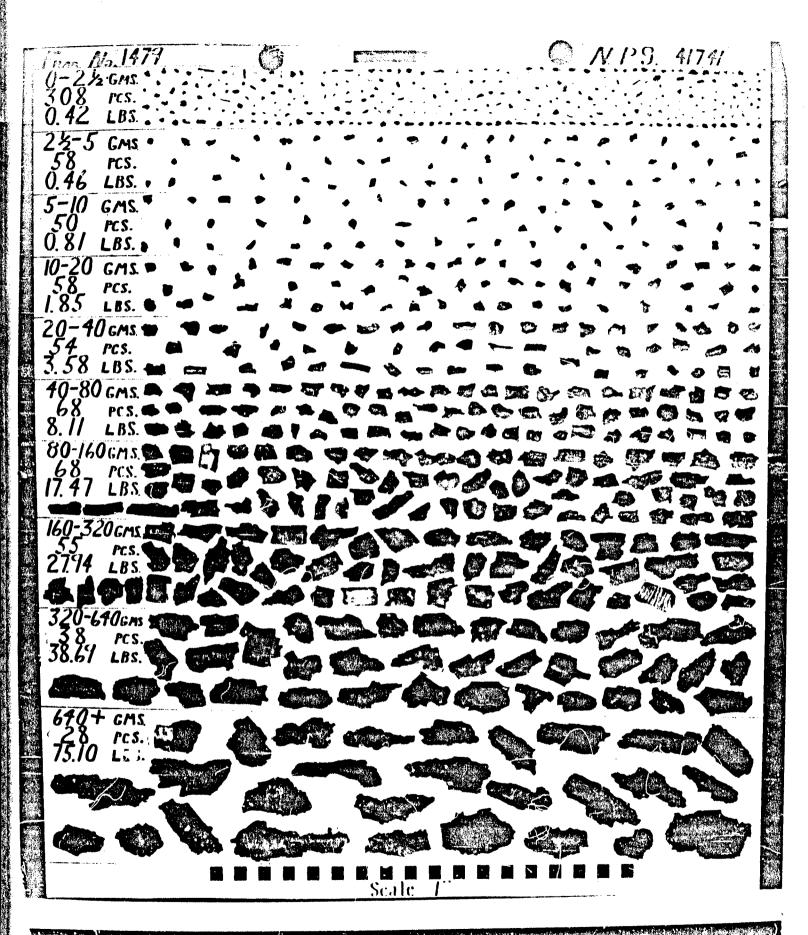
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MASS DESTRUMENTOR DATA

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THE PERSON NAMED IN	3	본취	2.21	0.89	1.3	88.0	1.22	Down) 0.29
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	ŝ	. e	Zone 60° - 120° 1 936.2 79.4	2 935.2 79.4 0.89 1417 0.62 81 1.02 61 1.95 3 934.2 79.4 0.87 876 0.92 125 1.50 101 2.86	Total Eds. 2 and 3 1869.5 158.8 1.76 2293 1.54 206 2.52 162 4.83 155	Average Eds. 2 and 3 934.7 79.4 0.88	Zone 150° - 180° (Base Down) 4 934.2 79.4 1.22 2034 0.84 121 1.17 79 1.78 59	Zons 0° - 30° (Hose Dorn) 5 936.2 79.4 0.29
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COMPIDENTIAL SECTION INFORMATION

APPENDIX B

THE II

MASS DISTRIBUTION DATA

PRIGHT MASS DISTUBUTION, "ATTR PIT RECOVER, 14" HE PROJECTIES ME 19-4 KIPLOSIVE "D" LOADED

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312.6	1,18	92	1.2	55	2.33	77	5.27 171		12.13	3 182 2	97.0	167	42.75	168.	168 74,01	77	102,38	163	102,38 103 255.73	104		,	517,62	2008	•
104.2		C.39 254	C.41		52 0.76 47 1.76 57	1.7	1.78		70-7	19	8.82	*	56 14.25 56 24.67	*	24.67	L7	11.13	ጸ	34 85.24	35		•	172.54	639	•

APPENDIX B

TABLE III

FRAGMENT VELOCITY DATA

Base Line: 80 feet 35mm Fastax Camera Rd. 1 - 12" HC Mk 17-2 Total Weight 936.2 lbs.

3120 frames per sec. Filler: Explosive "D" Filler Weight 79.4 lbs.

113 2 2210 114 2 2190 115 2 2170 116 2 2150 117 2 2130 119 4 2100 120 3 2080 121 2 2060 122 2 2050
115 2 2170 116 2 2150 117 2 2130 119 4 2100 120 3 2080 121 2 2060
115 2 2170 116 2 2150 117 2 2130 119 4 2100 120 3 2080 121 2 2060
116 2 2150 117 2 2130 119 4 2100 120 3 2080 121 2 2060
117 2 2130 119 4 2100 120 3 2080 121 2 2060
119 4 2100 120 3 2080 121 2 2060
120 3 2080 121 2 2060
121 2 2060
122 2 2050
123 1 2030
127 2 1970
127 2 1970 128 1 1950
120
Median 2110
Average 21CO

TABLE III (Continued)

Base Line: 80 feet 35mm Fastax Camera Rd. 2 - 12" HC Mk 17-2 Total Weight 935.2 lbs.

3420 frames per sec. Filler: Explosive "D" Filler Weight 79.4 lbs.

Frame in Which Hit Occurred		one 91° - 104° No. Fragments	Velocity (f/s)
124 126 127 128 129 130 131	•	2 1 1 2 3 1 2	2210 2170 2150 2140 2120 2100 2090 2070
Median			2130 2130

TABLE III (Continued)

Base Line: 80 feet 35mm Fastax Camera Rd. 3 - 12" HC Mk 17-2 Total Weight 934.2 lbs.

3140 frames per sec. Filler: Explosive "D" Filler Weight 79.4 lbs.

Frame in Which Hit Occurred	Zone 91° - 104° No. Fragments	Velocity (f/s)
113 114 115 116 117 118 119 121 122 123 124	2 3 3 2 1 1 1 2	2220 2200 2180 2170 2150 2130 2110 2080 2060 2040 2030
Median Average		2170 2140

TABLE IV

FRAGMENT VELOCITY DATA

Base Line: 80 feet 35mm Fastax Camera Rd. 2 - 14" HC Mk 19-4 Total Weight 1268.4 lbs.

2100 frames per sec. Filler: Explosive "D" Filler Weight 104.2 lbs.

Frame in Which Hit Occurred	No. Fragments	Velocity (f/s)
73 74 76 77 78 87 88 89	2 2 1 1 1 1	2300 2270 2210 2180 2150 1930 1910 1890
Median Average		2230 2150

TABLE IV (Continued)

Base Line: 80 feet 35mm Fastax Camera Rd. 3 - 14" HC Mk 19-4 Total Weight 1272.3 1bs.

3030 frames per sec. Filler: Explosive "D" Filler Weight 104.2 lbs.

Frame in Which Hit Occurred	No. Fragments	Velocity (f/s)
106 107 108 109 110 112 113 115 116	121232132	2290 2270 2240 2220 2200 2160 2150 2110 2090 2070
Median Average		2190 2170

Metallurgical Examination of Fragments from 12" HC Projectiles Nos. 1421 (Rd. No. 1), 1422 (Rd. No. 2). and 1423 (Rd. No. 3)

Chemical Composition:

A heavy fragment (320-640 grams) from each projectile was analyzed.

Projectile Number	<u>c</u>	Mn	P_		<u> 51</u>	N1	Cr	Mo
1421	.45	1.68	.030	.018	.19	.28	•98	under .10
1422	.41	1.55	.023	.011	.23	.19	•92	under .10
1423	.44	1.64	.028	.019	.23	.22	•98	under .10

There were no significant differences in the chemical composition of the three (3) projectiles. The steel was a manganese-chromium alloy type with residual nickel and molybdenum.

Hardness:

A fragment from the 160-320 grams group and from the 320-640 grams group of each projectile was sectioned and Vickers hardness tests were made on relatively undisturbed metal near the outside wall of the projectile.

Projectile Number	Vickers Hardness 160-320 gms. Group	Number (20 kg.) 320-640 gms. Group
1421 1422	260 274	253 279
1423	296	315

Projectile No. 1421, which showed the finer fragmentation, apparently was a little softer than either of the other projectiles. However, Nos. 1422 and 1423 had a considerable difference in hardness which nevertheless did not affect their relative performance.

Impact Strength:

Charpy V-notch impact tests were made using 5 x 10 x 55 mm. specimens propared from the larger fragments by selective machining. The test bars were cut longitudinal to the projectile axis and

Metallurgical Examination of Fragments from 12" HC Projectiles Nos. 1421 (Rd. No. 1), 1422 (Rd. No. 2). and 1423 (Rd. No. 3) (Continued)

were notched tangential to the projectile diameter on a 5mm face. In spite of some difficulties indicated by the data in Table (M-1), the results appeared to be significant particularly with regard to the estimation of per cent grain on the fracture surfaces. The test values were plotted in Figure (M-1) to show the relation between impact strength and temperature.

The estimated transition temperatures for 50% grain--50% shear fractures were as follows:

Projectile Number	Transition Temperature (50% shear fracture)
1421	+155°C
1422	+ 90°C
. 1423	+100°C

Measured by the high transition temperatures, all three (3) projectiles would be classed as "temper brittle" but the relatively higher transition temperature observed for the steel of Projectile No. 1421 indicated a comparatively greater tendency toward brittle failure than for the other two (2) projectiles.

Macrostructure:

The fragments of Projectile No. 1421 tended to show a relatively greater tendency toward internal cracking as illustrated by the unetched section in Figure (M-2). The predominant mode of fracture was a radial type of cracking probably caused by tensil stresses in the expanding side wall at the beginning of detonation.

The macrostructure of the etched sections is illustrated in Figure (N-3). The fragments from Nos. 1421 and 1422 HC Projectiles showed both the original cast dendritic structure near the outer wall and the worked structure from forging along the inside wall. The No. 1423 fragment had a more extensively worked structure such as might have occurred near the base of the projectile.

Metallurgical Examination of Fragments from 12" HC Projectiles Nos. 1421 (Rd. No. 1) 1422 (Rd. No. 2). and 1423 (Rd. No. 3) (Continued)

Microstructure:

The photomicrographs in Figure (M-4) indicated a quenched and tempered microstructure.

Projec- tile Number Microstructure		Inclusion Rating (ASTM Globular Oxides)	Austenitic Grain <u>Size</u>	McQuaid- Ehn Grain Size	
1421	Fully tempered structure.	No. 2 - thin	3-4	2-3	
1422	Less tempered than #1421.	No. 4 - thin	3-4	3	
1423	Less tempered than #1422 (and #1421).	No. 4 - thick	3-4	2	

The amount of tempering decreased in the following order: #1421 - #1422 - #1423. This change corresponded to a gradual increase in hardness as indicated by the values given in Figure (N-4).

The inclusion rating, although based on a limited sample size, showed a gradual increase of inclusion content in the order: #1421 - #1422 - #1423.

A coarse grain size was observed in all three (3) samples.

Discussion:

The body of the 12" HC Projectile No. 1421--with the most desirable fragment distribution--was softer, had a more ductile microstructure and was a cleaner steel than that of the other test projectiles. However, Projectile No. 1422, which was intermediate in these same respects, had a fragment mass distribution almost exactly like that of No. 1423 and not at all like No. 1421. The only respect in which the latter projectile was observed to differ appreciably from the other two (2) projectiles was in the greater tendency toward brittle failure shown by the impact test.

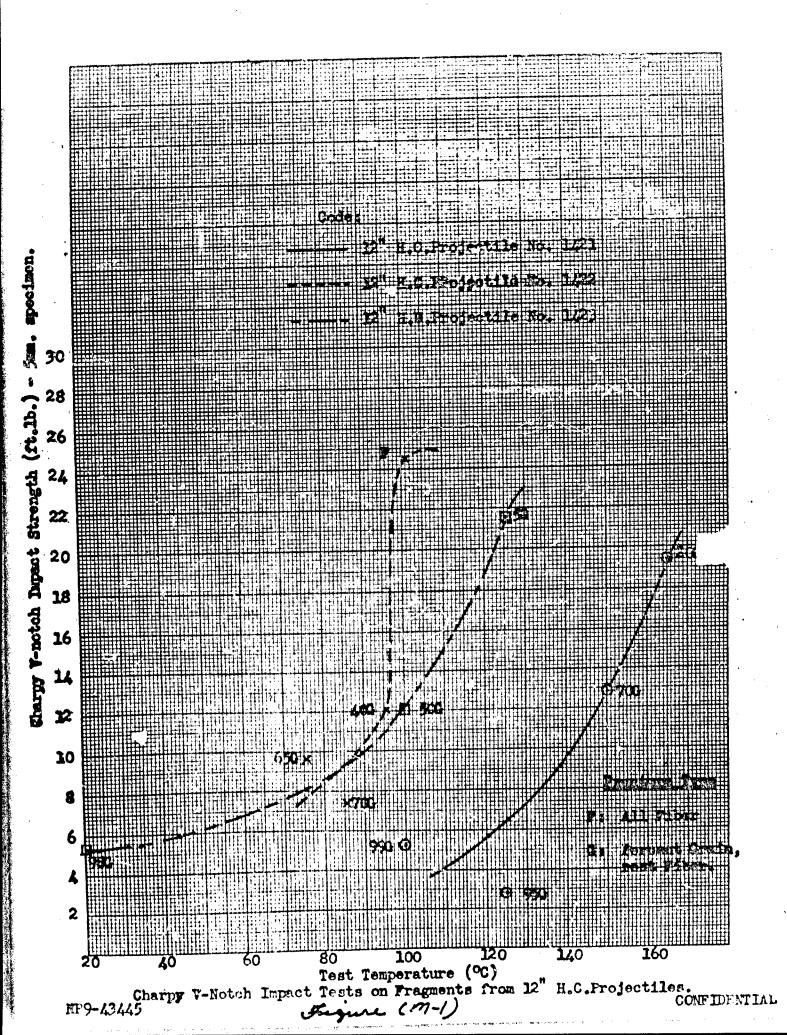
Metallurgical Examination of Fragments from 12" HC Projectiles Nos. 1421 (Rd. No. 1) 1422 (Rd. No. 2). and 1423 (Rd. No. 3) (Continued)

The other projectile steels were also temper brittle by ordinary standards without causing unusual fragmentation but it is possible that the relatively high order of brittleness in Projectile No. 1421 could have exceeded some critical value above which fragmentation might be affected. The finer fragmentation of 12" HC Projectile No. 1421 therefore may have been associated with a relatively greater tendency toward brittleness shown by the impact test.

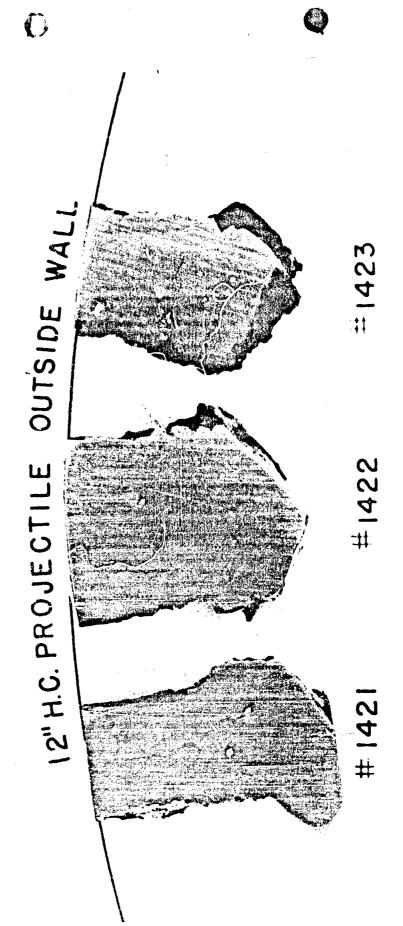
Table (M-1) Charry V-notch Impact Strength of Fragments from 12" HC Projectiles

Standard except fun wide instead of 10mm 30 ft.1b. capacity, velocity 15.12 ft. per second Spootmens:

Remarks		Only 1/2 of section showed	fresh fracture						•	Only 3/4 of	section showed frosh fracture
Fracture Rating	95% grain 99% grain	70% grain	20% grain	65% grain	All fiber	70% grain	40% grain	50% grain	5% grain	98% grain	
Charpy Impact Str.(ft/1b)	2°8 2°8	12.9	19.4	7.6	9.7%	7.3	12.0	12.0	27.5	5.3	
Test Temp.(°C)	+125	+150	+165	+ 75	+100	+ 85	+ 95	+100	+125	+ 22	
Magneflux Inspection Before Testing	No cracks Longitudinal cracks on	back of test specimen Light transferse cracks	No cracks	Longitudinal cracks on	No cracks	Bad crack at root	of notch				
Test No.	H &	w.	4	н	. ~	m	7	н	ત	М	
Projectile	1751			1722				1,23			

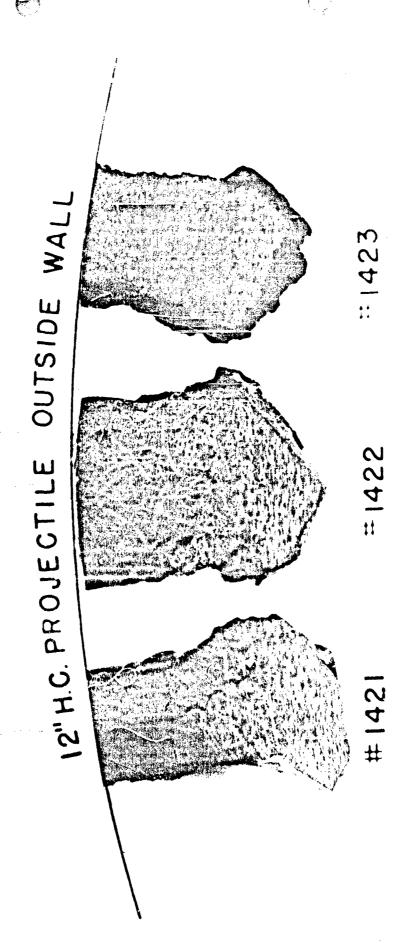


Transverse Sections Through Typical Fragments in the 320-640 gms. Group, Showing Location of Fracture. Unetched NP9-43406

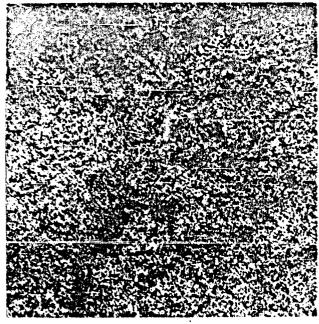


Macrostructure of Transverse Sections Through Typical Fragments in the 320-640 gms. Group Showing the Magnification: 1 1/2 X

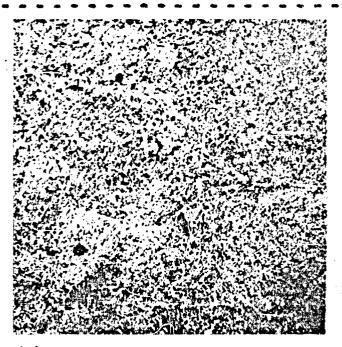
Etch: Ammonium persulfate



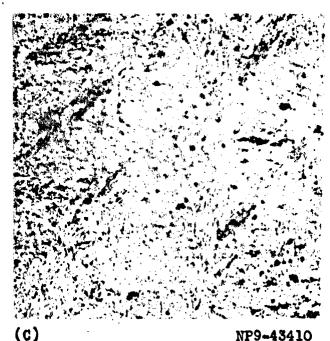




(A) NP9-43408
Projectile No. 1421
Hardness: 262 VPN (10 kg)



(B) NP9-43409
Projectile No. 1422
Hardness: 283 VPN (10 kg)



Projectile No. 1423 Hardness: 312 VPN (10 kg)

Microstructures in Side Wall Fragments from Three 12th HC Projectiles,
Longitudinal Sections of 160-320 gms. Group.

Etch: Nital-picral. Magnification: 250X



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Major Caliber HC Projectiles

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